

# Numerical approach to a rate-independent model of decohesion in laminated composites

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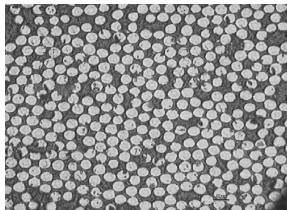
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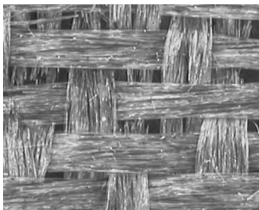
PANM 15: Programy a algoritmy numerické matematiky 15  
6.–11. června, Dolní Maxov

# Interfaces in composite materials

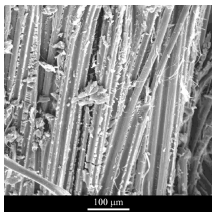
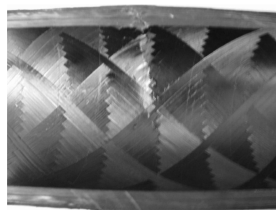
**Microscale**



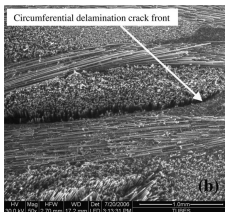
**Mesoscale**



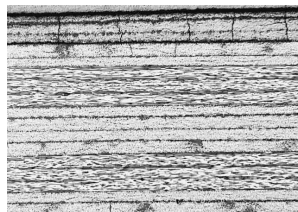
**Macroscale**



$\approx 10 \mu\text{m}$



$\approx 1 \text{ mm}$



$\approx 1 \text{ dm}$

**Essential aspect for reliable design of composite structures**

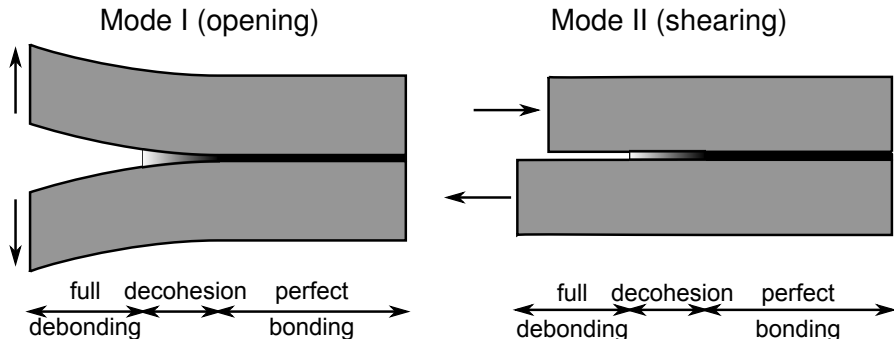
(Macroscopic delamination)



- **Energy-based framework**
- Decohesion  $\equiv$  displacement jumps at interfaces
- Inelastic phenomena concentrated at interfaces
- Rate-independent (quasi-static) approximation
- Frictionless contact conditions
- Small-strain setting

# Basic concepts of interfacial damage mechanics

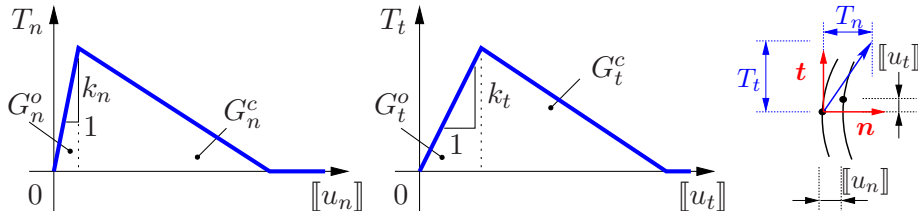
## Constitutive characterization



- Initial stiffnesses:  $k_n, k_t$  ( $\text{Nm}^{-3}$ )
- Activation energies:  $G_n^o, G_t^o$  ( $\text{Jm}^{-2}$ )
- Dissipated energies:  $G_n^c, G_t^c$  ( $\text{Jm}^{-2}$ )
- Mode interaction parameters

# Basic concepts of interfacial damage mechanics

## State variables



- Displacement jump decomposition

$$[[u_n]] = [[\mathbf{u}]] \cdot \mathbf{n} \geq 0 \quad [[u_t]] = \| [[\mathbf{u}]] - [[u_n]] \mathbf{n} \| \quad (1)$$

- Intensity of adhesion

$$T_n = \zeta k_n [[u_n]] \quad T_t = \zeta k_t [[u_t]] \quad 0 \leq \zeta \leq 1$$

# Basic concepts of interfacial damage mechanics

Interaction criteria (VALOROSO & CHAMPANEY, 2006)

- Mode mixity parameter

$$\psi(\llbracket \mathbf{u} \rrbracket) = \sqrt{\frac{k_t}{k_n} \frac{\llbracket u_t \rrbracket}{\llbracket u_n \rrbracket}} \quad (\text{mode I} \Rightarrow) 0 \leq \psi < +\infty (\text{= mode II})$$

- Mode interaction criteria

$$\left( \frac{G^o(\psi)}{(1 + \psi^2)G_n^o} \right)^{a_1} + \left( \frac{\psi^2 G^o(\psi)}{(1 + \psi^2)G_t^o} \right)^{a_2} = 1$$
$$\left( \frac{G^c(\psi)}{(1 + \psi^2)G_n^c} \right)^{b_1} + \left( \frac{\psi^2 G^c(\psi)}{(1 + \psi^2)G_t^c} \right)^{b_2} = 1$$

parameters  $a_1, a_2, b_1, b_2$  fitted from experiments or taken as 2

# Motivation

Challenges in modelling delamination phenomena

## Theoretical aspects

- 1 No supporting existence theory for mixed-mode description
- 2 (At least) abstract approximation results

## Computational aspects

- 1 Oscillations of interfacial tractions for almost perfect interfaces ( $k_{\bullet} \rightarrow \infty$ )
- 2 Unstable response for brittle interfaces, leading to oscillation of quantity of interests for coarse meshes
- 3 Efficient and reliable resolution of frictionless contact

- 1 Energetic rate-independent systems
  - Energetic solution
  - Incremental energy minimization
  - Existence and approximation results
  - Application to delamination problem
- 2 Numerical treatment
  - Incremental optimization problems
  - Alternate minimization
  - Backtracking strategy
  - Application of FETI-based methods
- 3 Examples
- 4 Summary and outlook



# Energetic rate-independent systems

Notation (MIELKE, LEVITAS & THEIL, 2002; MIELKE & ROSSI, 2007)

- Domain  $\Omega \subset \mathbb{R}^d$ , time interval  $\mathbb{I} = [0; T]$
- State variables:  $\mathbf{q} = (\mathbf{u}, \mathbf{z}) \in \mathcal{Q} = \mathcal{U} \times \mathcal{Z}$ 
  - Displacements  $\mathbf{u} : \Omega \rightarrow \mathbb{R}^d$
  - Internal variables  $\mathbf{z} : \Omega \rightarrow \mathbb{R}^m$
- Constitutive description
  - Stored energy  $E(t, \mathbf{q}) : \mathbb{I} \times \mathcal{Q} \rightarrow \bar{\mathbb{R}}$
  - Dissipation rate  $D(\mathbf{q}, \dot{\mathbf{z}}) : \mathcal{Q} \times \mathcal{Q} \rightarrow [0; +\infty]$   
**State-dependent**  
positively 1-homogeneous  $\rightarrow$  rate-independence
- Stable sets

$$\mathcal{S}(t) = \{\mathbf{q} \in \mathcal{Q} : E(t, \mathbf{q}) \leq E(t, \tilde{\mathbf{q}}) + D(\mathbf{q}, \tilde{\mathbf{z}} - \mathbf{z}) \text{ for all } \tilde{\mathbf{q}} \in \mathcal{Q}\}$$

# Energetic rate-independent systems

Energetic solution (MIELKE and co-workers, 2002—)

## Energetic solution

Given  $\mathbf{q}(0) \in \mathcal{Q}$ , the process  $\mathbf{q} : \mathbb{I} \rightarrow \mathcal{Q}$  is an *energetic solution* to the rate-independent system  $(\mathcal{Q}, E, D)$  if for all  $t \in \mathbb{I}$  we have

- **Stability**

$$\mathbf{q}(t) \in \mathcal{S}(t)$$

- **Energy inequality**

$$E(t, \mathbf{q}(t)) + \int_0^t D(\mathbf{q}(s), \dot{\mathbf{z}}(s)) ds \leq E(0, \mathbf{q}(0)) + \int_0^t \partial_s E(s, \mathbf{q}(s)) ds$$

- Available existence results either assume  $D(\mathbf{q}, \dot{\mathbf{z}}) = D(\mathbf{z}, \dot{\mathbf{z}})$  or rely on a uniform convexity of  $E(t, \cdot)$  (MR, 2007)

# Energetic rate-independent systems

Incremental energy minimization (MIELKE and co-workers, 2002—)

- Rothe method

$$\mathcal{P}_\tau = \{0 = t_\tau^0 < t_\tau^1 < \dots < t_\tau^M = T\} \quad \text{with} \quad \tau = \max_{j=1, \dots, M} \{t_\tau^j - t_\tau^{j-1}\}$$

## Incremental problems

Given  $\mathbf{q}_\tau^0 = \mathbf{q}(0) \in \mathcal{Q}$ , solve for  $k = 1, \dots, M$

$$\mathbf{q}_\tau^k \in \arg \min_{\mathbf{q} \in \mathcal{Q}} E(t_k, \mathbf{q}) + D(\mathbf{q}_\tau^{k-1}, \mathbf{z} - \mathbf{z}_\tau^{k-1}) \quad (2)$$

- Used to show convergence as  $\tau \rightarrow 0$
- Provides convenient basis for numerical treatment (ORTIZ & STAINIER, 1999 —)

# Energetic rate-independent systems

Existence results (MIELKE and co-workers, 2002—; KRUŽÍK & ZEMAN, in preparation)

## Assumptions (Stored energy)

- $E(t, \cdot)$  is weakly lower semicontinuous and coercive

$$E(t, \mathbf{q}) < \infty \Rightarrow |\partial_t E(t, \mathbf{q})| \leq C_0(C_1 + E(t, \mathbf{q}))$$

- $\partial_t E(t, \cdot)$  is weakly continuous for all  $t \in \mathbb{I}$  and satisfies

$$|\partial_t E(t_1, \mathbf{q}) - \partial_t E(t_2, \mathbf{q})| \leq \omega(|t_1 - t_2|)$$

for a non-decreasing  $\omega : \mathbb{I} \rightarrow \mathbb{R}_0^+$

# Energetic rate-independent systems

Existence results (MIELKE and co-workers, 2002—; KRUŽÍK & ZEMAN, in preparation)

## Assumptions (Dissipation + “Compatibility”)

- For all  $z \in \mathcal{Z}$  and  $q_1, q_2, q_3 \in \mathcal{Q}$

$$C_0 \|z_1 - z_2\|_{\mathcal{X}} \leq D(q_1, z_2 - z_1)$$

$$|D(q_1, z) - D(q_2, z)| \leq C_1 \|q_2 - q_1\|_{\mathcal{Q}} \|z\|_{\mathcal{Z}}$$

$$D(q_1, z_3 - z_1) \leq D(q_1, z_2 - z_1) + D(q_1, z_3 - z_2)$$

where  $\mathcal{Z} \in \mathcal{X}$

- For each sequence  $\{(t_n, q_n)\}_{n \in \mathbb{N}}$  with  $q_n \in \mathcal{S}(t_n)$  and  $t_n \rightarrow t^*$  and  $q_n \rightarrow q^*$  and  $\sup_n E(t_n, q_n) < \infty$  it holds

$$q_* \in \mathcal{S}(t^*) \quad \partial_t E(t^*, q^n) \rightarrow \partial_t E(t^*, q^*)$$

# Energetic rate-independent systems

Existence results (MIELKE and co-workers, 2002—; KRUŽÍK & ZEMAN, in preparation)

- Solution of the incremental problem exists for all  $k$  and  $\tau$  and is stable
- It satisfies a-posteriori two-sided energy estimates

$$\int_{t_\tau^{k-1}}^{t_\tau^k} \partial_s E(s, \mathbf{q}_\tau^k) \, ds \leq E(t_\tau^k, \mathbf{q}_\tau^k) - E(t_\tau^{k-1}, \mathbf{q}_\tau^{k-1}) \quad (3)$$
$$+ D(\mathbf{q}_\tau^{k-1}, \mathbf{z}_\tau^k - \mathbf{z}_\tau^{k-1}) \leq \int_{t_\tau^{k-1}}^{t_\tau^k} \partial_s E(s, \mathbf{q}_\tau^{k-1}) \, ds$$

- As  $\tau \rightarrow 0$ , there exist  $\mathbf{z} \in BV(\mathbb{I}; \mathcal{X})$  and  $\mathbf{u}(t) : \mathbb{I} \rightarrow \mathcal{U}$  such that

$$(\mathbf{u}(t), \mathbf{z}(t)) \in \mathcal{S}(t) \quad \text{and} \quad \widehat{\mathbf{z}}_\tau \rightarrow \mathbf{z} \text{ in } BV(\mathbb{I}; \mathcal{X})$$

and the process satisfies the energy inequality.

# Energetic rate-independent systems

Abstract approximation result (MIELKE & ROUBÍČEK, 2009)

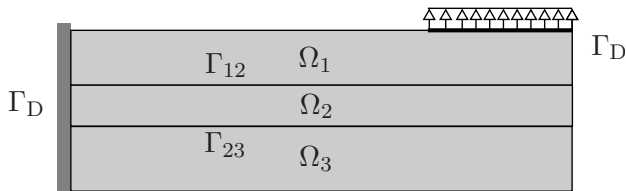
## Energetic density of $\mathcal{Q}_h \subset \mathcal{Q}$

For each  $(t, \mathbf{q}) \in \mathbb{I} \times \mathcal{Q}$ , there exists  $\{\mathbf{q}_h\}$  such that  $\mathbf{q}_h \in \mathcal{Q}_h$ ,  $\mathbf{q}_h \rightarrow \mathbf{q}$  and  $E(t, \mathbf{q}_h) \rightarrow E(t, \mathbf{q})$

- Incremental energy minimization yields stable approximate solution  $\{\mathbf{q}_{\tau,h}^k\}$
- Approximate solutions  $\{\mathbf{q}_{\tau,h}^k\}$  satisfy the two-sided energy estimate
- If  $\mathcal{Q}_h$  satisfies adjusted compatibility condition, the solution converges to an energetic solution as  $\tau \rightarrow 0$  and  $h \rightarrow 0$

# Application to delamination problem

Geometry (KOČVARA, MIELKE & ROUBÍČEK, 2006)



- Body  $\Omega \subset \mathbb{R}^d$  with the Lipschitz boundary  $\Gamma$
- Time-dependent Dirichlet boundary conditions at  $\Gamma_D$
- Collection of disjoint bodies  $\Omega_\alpha$  with Lipschitz boundaries  $\Gamma_\alpha$ ,  $\alpha = 1, 2, \dots, m$  ( $\Gamma_{D,\alpha} = \Gamma_\alpha \cap \Gamma_D \neq \emptyset$ )
- Internal boundaries  $\Gamma_{\alpha\beta} = \Gamma_\alpha \cap \Gamma_\beta$  ( $\alpha > \beta$ ) with normal vectors  $\mathbf{n}_{\alpha\beta}$



# Application to delamination problem

State variables and data (KOČVARA, MIELKE & ROUBÍČEK, 2006; KRUŽÍK & ZEMAN)

- Domain displacements  $\mathbf{u}_\alpha : \Omega_\alpha \rightarrow \mathbb{R}^d$
- Internal variable  $\zeta_{\alpha\beta} : \Gamma_{\alpha\beta} \rightarrow \mathbb{R}$
- Function spaces

$$\mathcal{U} = \prod_{\alpha=1}^m \left\{ \mathbf{u}_\alpha \in W^{1,2}(\Omega_\alpha; \mathbb{R}^d), \mathbf{u}_\alpha|_{\Gamma_{D\alpha}} = \mathbf{0} \right\}$$

$$\mathcal{Z} = \prod_{\alpha=1}^m \prod_{\beta=\alpha+1}^m \left\{ \zeta_{\alpha\beta} \in W^{1,2}(\Gamma_{\alpha\beta}) \right\}$$

$$\mathcal{X} = \prod_{\alpha=1}^m \prod_{\beta=\alpha+1}^m \left\{ \zeta_{\alpha\beta} \in L^1(\Gamma_{\alpha\beta}) \right\}$$

- Hard-device loading  $\mathbf{w}_D \in C^1(\mathbb{I}; W^{1/2,2}(\Gamma_D; \mathbb{R}^d))$

# Application to delamination problem

Stored energy (KOČVARA, MIELKE & ROUBÍČEK, 2006; KRUŽÍK & ZEMAN)

- Stored energy

$$E(t, \mathbf{q}) = \sum_{\alpha=1}^m E_{\alpha}(t, \varepsilon(\mathbf{u}_{\alpha})) + \sum_{\alpha=1}^m \sum_{\beta=\alpha+1}^m E_{\alpha\beta}(\mathbf{u}_{\alpha} - \mathbf{u}_{\beta}, \zeta_{\alpha\beta})$$

- Bulk energy

$$E_{\alpha}(t, \varepsilon) = \frac{1}{2} \int_{\Omega_{\alpha}} \mathbf{C}_{\alpha} (\varepsilon + \varepsilon(\mathbf{u}_{D,\alpha}(t))) : (\varepsilon + \varepsilon(\mathbf{u}_{D,\alpha}(t))) \, d\Omega$$

- Interfacial energy from (1)

$$E_{\alpha\beta}(\llbracket \mathbf{u} \rrbracket, \zeta) = \begin{cases} \int_{\Gamma_{\alpha\beta}} \frac{\zeta}{2} \mathbf{k}_{\alpha\beta} \llbracket \mathbf{u} \rrbracket \cdot \llbracket \mathbf{u} \rrbracket + f_{\alpha\beta}(\psi(\llbracket \mathbf{u} \rrbracket), \zeta) + \frac{\kappa}{2} (\zeta')^2 \, d\Gamma \\ \text{for } \llbracket \mathbf{u} \rrbracket_n \geq 0 \text{ and } 0 \leq \zeta \leq 1 \text{ a.e. on } \Gamma_{\alpha\beta} \\ +\infty \text{ otherwise} \end{cases}$$

# Application to delamination problem

Dissipation function (KOČVARA, MIELKE & ROUBÍČEK, 2006; KRUŽÍK & ZEMAN)

- Dissipation rate

$$D(\mathbf{q}, \dot{\mathbf{z}}) = \sum_{\alpha=1}^m \sum_{\beta=\alpha+1}^m D_{\alpha\beta}(\mathbf{u}_{\alpha} - \mathbf{u}_{\beta}, \zeta_{\alpha\beta}, \dot{\zeta}_{\alpha\beta})$$

- Interfacial dissipation

$$D_{\alpha\beta}([\mathbf{u}], \zeta, \dot{\zeta}) = \begin{cases} - \int_{\Gamma_{\alpha\beta}} G_{\alpha\beta}^c(\psi([\mathbf{u}])) \dot{\zeta} \, d\Gamma & \text{for } \dot{\zeta} \leq 0 \\ +\infty & \text{otherwise} \end{cases}$$

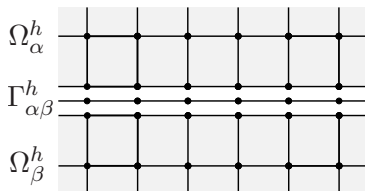
- (KMR, 2006)  $\Rightarrow$  Existence of energetic solution
- (MR, 2009)  $\Rightarrow$  Approximation results for state-independent dissipation and for discretization with  $\mathcal{U}$  with  $P_1$  elements and  $\mathcal{Z}$  with  $P_0$  elements

# Numerical treatment

## Strategy and algebraic re-formulation

- General strategy

- Reduce numerics to interfaces  $\rightarrow$  FETI-family methods (DOSTÁL, 2009)



- Discrete state variables

- Nodal displacements:  $u_\alpha$
- Interfacial displacement jumps:  $\llbracket u_{\alpha\beta} \rrbracket$
- Adhesion intensity variables:  $z_{\alpha\beta}$

$$(u, \llbracket u \rrbracket) \in \mathbb{K}^u = \{(v, \llbracket v \rrbracket) : B_d v = 0, B_e v = \llbracket v \rrbracket, B_i \llbracket v \rrbracket \geq 0\}$$

$$z \in \mathbb{K}^z = \{y : 0 \leq y \leq 1\}$$

# Numerical treatment

## Discrete energy functions

- Energy stored in domains

$$E_{\Omega,h}(t, \mathbf{u}) = \frac{1}{2} (\mathbf{u} + \mathbf{u}_D(t))^T \mathbf{K} (\mathbf{u} + \mathbf{u}_D(t)) \quad \mathbf{K} = \begin{bmatrix} \mathbf{K}_1 & & \\ & \ddots & \\ & & \mathbf{K}_m \end{bmatrix}$$

- Energy stored at interfaces

$$E_{\Gamma,h}([\mathbf{u}], \mathbf{z}) = \frac{1}{2} [\mathbf{u}]^T \mathbf{k}(\mathbf{z}) [\mathbf{u}] + f_h(\psi([\mathbf{u}]), \mathbf{z})$$

$f_h(\psi, \cdot)$  convex in  $\mathbf{z}$

- Interfacial dissipation:  $\mathbf{z} \leq 0$

$$D_h([\mathbf{u}], \mathbf{z}) = -\mathbf{g}(\psi([\mathbf{u}]))^T \mathbf{z}$$

# Numerical treatment

## Incremental optimization problems

- Incremental energy (2)

$$\begin{aligned} I_{k,h}(z, u, \llbracket u \rrbracket) &= \frac{1}{2} u^T K u + u^T K u_D(t_k) + \frac{1}{2} \llbracket u \rrbracket^T k(z) \llbracket u \rrbracket + f_h(\psi(\llbracket u \rrbracket), z) \\ &- z^T g(\psi(\llbracket u \rrbracket_{k-1})) \end{aligned}$$

## Incremental optimization problems

Given  $(z_0, u_0, \llbracket u \rrbracket_0) \in \mathbb{K}^z \times \mathbb{K}^u$  solve for  $k = 1, \dots, M$

$$(z_k, u_k, \llbracket u \rrbracket_k) = \arg \min_{0 \leq z \leq z_{k-1}} \min_{(u, \llbracket u \rrbracket) \in \mathbb{K}^u} I_{k,h}(z, u, \llbracket u \rrbracket)$$

- Large-scale, sparse, separately convex and constrained problem

# Numerical treatment

Incremental minimization (BOURDIN, FRANCFORT & MARIGO, 2000; BOURDIN, 2007)

- Alternate minimization algorithm ( $\equiv$  staggered scheme)

## Alternate minimization algorithm

- 1: Set  $j = 0$ ,  $\mathbf{z}^{(0)} = \mathbf{z}_{k-1}$ ,  $\mathbf{u}^{(0)} = \mathbf{u}_{k-1}$ ,  $\llbracket \mathbf{u} \rrbracket^{(0)} = \llbracket \mathbf{u} \rrbracket_{k-1}$
- 2: **repeat**
- 3:   Set  $j = j + 1$
- 4:   Solve  $(\mathbf{u}^{(j)}, \llbracket \mathbf{u} \rrbracket^{(j)}) = \arg \min_{(\mathbf{u}, \llbracket \mathbf{u} \rrbracket) \in \mathbb{K}^u} I_{k,h}(\mathbf{z}^{(j-1)}, \mathbf{u}, \llbracket \mathbf{u} \rrbracket)$
- 5:   Solve  $\mathbf{z}^{(j)} = \arg \min_{0 \leq \mathbf{z} \leq \mathbf{z}_{k-1}} I_{k,h}(\mathbf{z}, \mathbf{u}^{(j)}, \llbracket \mathbf{u} \rrbracket^{(j)})$
- 6: **until**  $\|\mathbf{z}^{(j)} - \mathbf{z}^{(j-1)}\|_{\infty} \leq \delta$
- 7: Set  $\mathbf{u}_k = \mathbf{u}^{(j)}$ ,  $\llbracket \mathbf{u} \rrbracket_k = \llbracket \mathbf{u} \rrbracket^{(j)}$ ,  $\mathbf{z}_k = \mathbf{z}^{(j)}$

- Step 5 can be performed element-by-element at interface
- Step 4 well-suited for FETI-based solvers

# Numerical treatment

Backtracking strategy (MIELKE, ROUBÍČEK & ZEMAN, 2010; BENEŠOVÁ, 2009–)

- Convergence to a *critical point* of the objective function
- Not good enough – theory relies on the *global* minimization

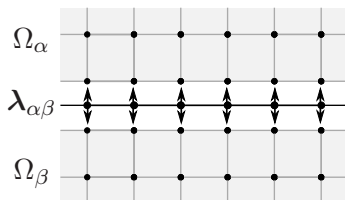
## Backtracking algorithm

```
1 : Set  $k = 1, z_{-1} = 1, z_0 = 1, z^{(0)} = 1$ 
2 : repeat
3 :   Determine  $z_k$  using the alternate minimization algorithm
   :   for time  $t_k$  and initial value  $z^{(0)}$ .
4 :   Set  $z^{(0)} = z_k$ 
5 :   if two-sided estimate (3) is satisfied with tolerance  $\eta$ 
6 :     Set  $k = k + 1$ 
7 :   else
8 :     Set  $k = k - 1$ 
9 :   end
10: until  $k \leq M$ 
```



# Numerical treatment

FETI formulation (FARHAT & ROUX, 1991; KRUIS & BITTNAR, 2008; DOSTÁL; 2009)



- Lagrange function

$$L(u, [\mathbf{u}], \lambda) = \frac{1}{2} \mathbf{u}^T \mathbf{K} \mathbf{u} + \frac{1}{2} [\mathbf{u}]^T \mathbf{k} [\mathbf{u}] - \mathbf{d}^T \mathbf{u} + \lambda^T (\mathbf{B}_e \mathbf{u} - \mathbf{u})$$

- Saddle-point problem

$$(u, [\mathbf{u}], \lambda) = \arg \max_{\lambda} \min_u \min_{\mathbf{B}_i[\mathbf{u}] \geq 0} L(u, [\mathbf{u}], \lambda)$$

- The “unresolved” box constraint  $\mathbf{B}_i[\mathbf{u}] \geq 0$  will be enforced by a heuristic active set strategy

# Numerical treatment

Dual problem (FARHAT & ROUX, 1991; KRUIS & BITTNER, 2008; DOSTÁL; 2009)

- Optimality conditions

$$\begin{aligned} \llbracket \mathbf{u} \rrbracket &= \mathbf{k}^{-1} \boldsymbol{\lambda} & \mathbf{u} &= \mathbf{K}^+ \left( \mathbf{d} - \mathbf{B}_e^T \boldsymbol{\lambda} \right) + \mathbf{R} \alpha \\ \mathbf{R}^T \left( \mathbf{d} - \mathbf{B}_e^T \boldsymbol{\lambda} \right) &= \mathbf{0} & \mathbf{B}_e \mathbf{u} - \llbracket \mathbf{u} \rrbracket &= \mathbf{0} \end{aligned}$$

- Eliminate primary variables  $\mathbf{u}$  and  $\llbracket \mathbf{u} \rrbracket$  ( $\mathbf{R}^T \mathbf{d} = \mathbf{0}$ )

$$\begin{bmatrix} \mathbf{B}_e \mathbf{K}^+ \mathbf{B}_e^T + \mathbf{k}^{-1} & -\mathbf{B}_e \mathbf{R} \\ -\mathbf{R}^T \mathbf{B}_e^T & \mathbf{0} \end{bmatrix} \begin{bmatrix} \boldsymbol{\lambda} \\ \alpha \end{bmatrix} = \begin{bmatrix} \mathbf{B}_e \mathbf{K}^+ \mathbf{d} \\ \mathbf{0} \end{bmatrix}$$

- Problem reduced to **interfaces** ✓
- **Efficiently** solvable using Projected Conjugate Gradient solvers
- Perfect bonding  $\mathbf{k}^{-1} \rightarrow \mathbf{0}$  ✓

# Numerical treatment

Active set strategy (GRUBER & ZEMAN, in preparation)



## 1 Contact detection algorithm

- Tag interfacial nodes as primal ( $\mathcal{P}$ ) or dual ( $\mathcal{D}$ )

$$[[\mathbf{u}]]_e = \mathbf{k}_e^{-1} \lambda_e$$

- For  $\mathcal{D}$  : determine contact nodes ( $\mathcal{C}$ ) from  $\lambda$
- For  $\mathcal{P}$  : determine contact nodes ( $\mathcal{C}$ ) from  $[[\mathbf{u}]]$
- For  $\mathcal{C}$  : enforce  $[[\mathbf{u}]]_n = 0$  by setting compliance to zero
- For  $\mathcal{P} - \mathcal{C}$  : enforce  $\lambda = 0$  by static condensation

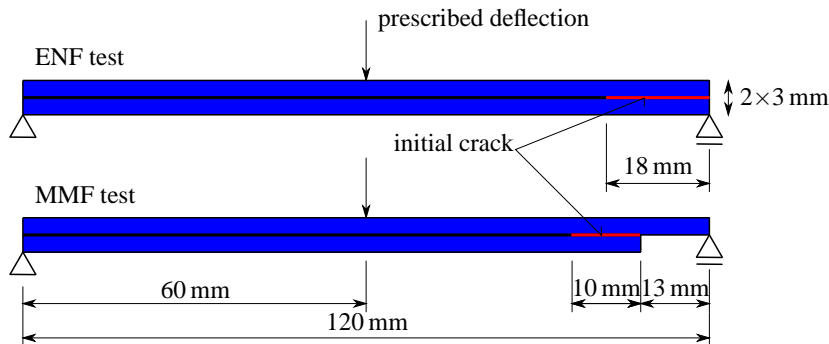
## 2 Solve dual system by standard Projected Conjugate Gradients

## 3 Check convergence of Lagrange multipliers $\lambda$

- Usually converges in 3–4 iterations ✓

# Examples

Notched flexure tests (VALOROSO & CHAMPANEY, 2006)



<i>Mesh size <math>h</math></i>	<i># of primal DOFs</i>	<i># of dual DOFs</i>
1 mm	1,936	242 (12%)
0.75 mm	3,220	322 (10%)
0.5 mm	6,748	482 (7%)

- $M = 40$  time steps

# Examples

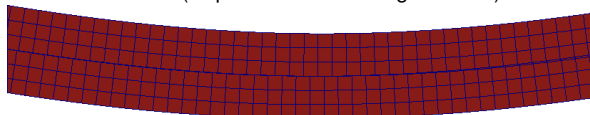
## Material data

- Domains:  $E = 75 \text{ GPa}$ ,  $\nu = 0.3$
- Interfaces: Piecewise linear interfacial law

<i>Material parameter</i>	<i>Ductile</i>	<i>Brittle</i>
$k_n = k_t \text{ (GNm}^{-3}\text{)}$	125	$125 \times 10^6$
$G_n^o = G_t^o \text{ (Jm}^{-2}\text{)}$	100	0.01
$G_n^c = G_t^c \text{ (Jm}^{-2}\text{)}$	250	25
Interaction parameters $a_i, b_i$	2	2

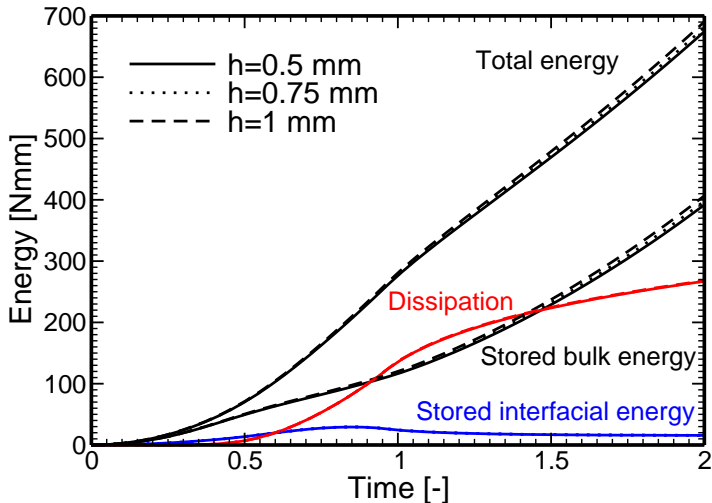
- Algorithmic settings:  $\delta = 10^{-5}$ ,  $\eta = 10^{-3}$
- In-house experimental MATLAB implementation

ENF test(displacements are magnified 5 $\times$ )



# Examples

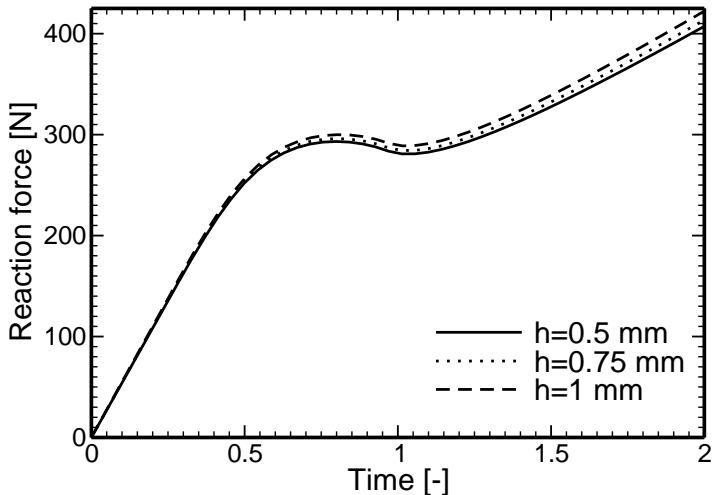
Energetics of ENF test,  $h \rightarrow 0$ , ductile interface, 60–300 s



(No back-tracking activated)

# Examples

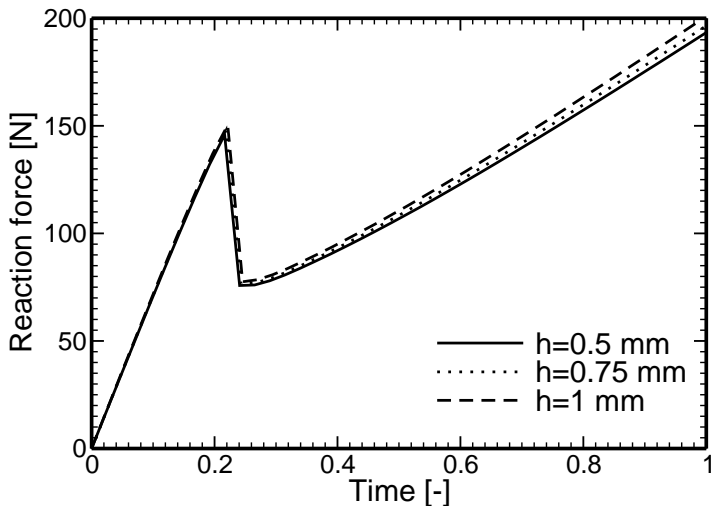
Force-displacement curves of ENF test,  $h \rightarrow 0$ , ductile interface, 60–300 s



(No back-tracking activated)

# Examples

Force-displacement curves of ENF test,  $h \rightarrow 0$ , brittle interface, 60–300 s



(Back-tracking inactive)



# Examples

ENF test, ductile interface, snapshots of delamination evolution



$t = 0.33$



$t = 0.66$



$t = 1.17$



$t = 1.50$



$t = 1.83$



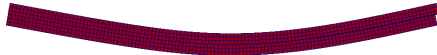
$t = 0.50$



$t = 1.00$



$t = 1.33$



$t = 1.67$

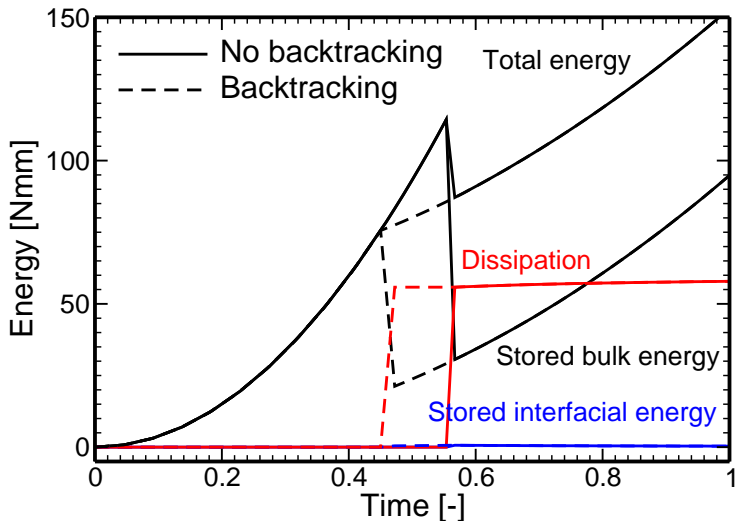


$t = 2$

Displacement are scaled  $5\times$

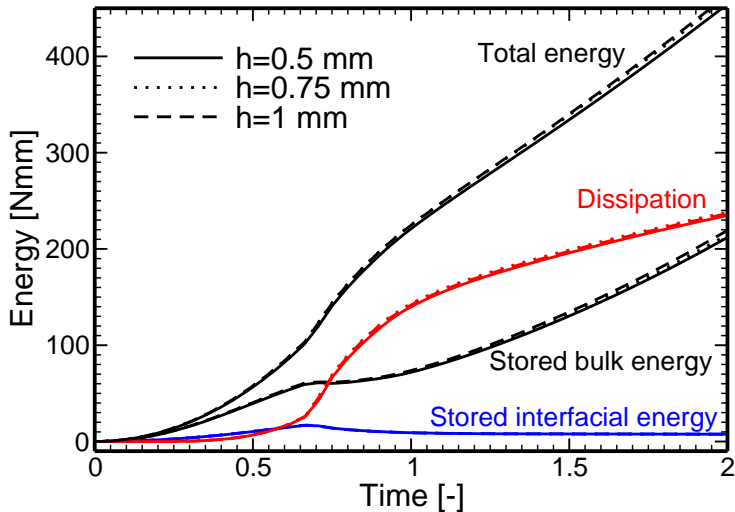
# Examples

Energetics of modified ENF test,  $h = 0.1$  mm, brittle interface



# Examples

Energetics of MMF test,  $h \rightarrow 0$ , ductile interface



(No back-tracking activated)

# Examples

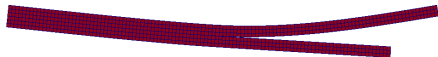
## Snapshots of MMF test



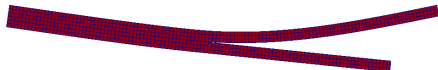
$t = 0.27$



$t = 0.62$



$t = 1.14$



$t = 1.48$



$t = 1.83$



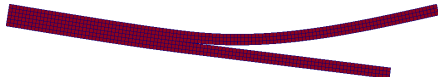
$t = 0.44$



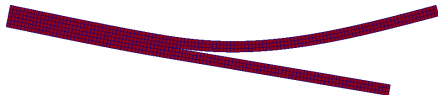
$t = 0.96$



$t = 1.31$



$t = 1.65$



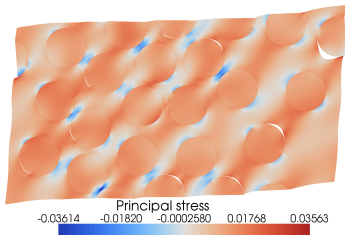
$t = 2$

Displacements are scaled  $5\times$

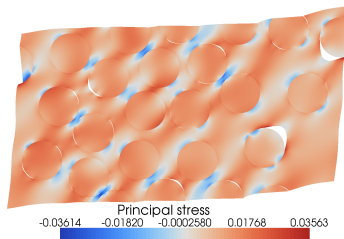
# Extensions

## Debonding in fibre-reinforced composites

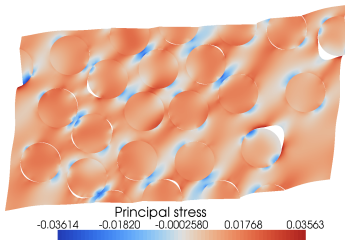
$t = 0.4$



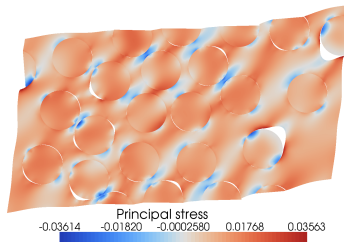
$t = 0.6$



$t = 0.8$

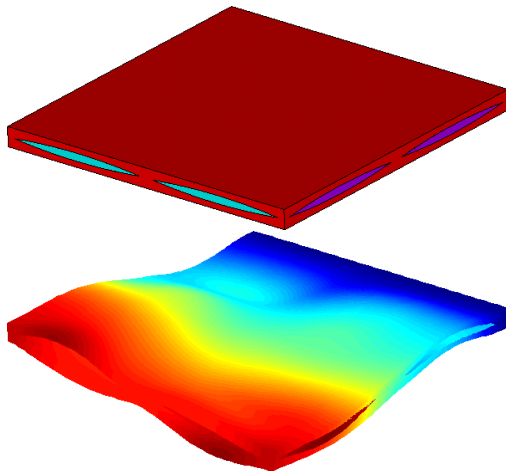


$t = 1$



# Extensions

Woven composites, preliminary results (courtesy of T. KOZUBEK, TU Ostrava)



- Analyzed using MATSOL library

# Summary and outlook

- Energetic framework
  - is well-suited for analysis of inelastic solid mechanics problems
  - provides background for efficient numerical implementation
  - addresses the problems of *stability* of solution when the response is non-unique
- FETI-based algorithm is well-suited for analysis in composite materials, even in sequential mode
- Future extensions
  - Abstract approximation results, homogenization
  - More efficient duality solvers
  - Application to woven composite materials

## Acknowledgements

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